

AMENDMENTS TO THE SPECIFICATION:

Please replace Paragraph [0007] with the following amended Paragraph:

Long, thin tools are used for extracting inflamed nerves. A manual treatment is commonly used to avoid breaking the extremely thin tools. Furthermore, the manual preparation is very time-consuming. Due to very different natural forms in the root canal, different tools must be used for each canal. The difference between the tools is in the length, conicity, diameter, flexibility and resistance. As such, extremely high strains of the tool are ~~used~~ realized, especially with regard to torsion and bending in curved root canals. Due to the special blade geometry of such rotating tools, the present device only needs low rotation speeds from 5 to 25 rotations per sec (300 to 2100 rotations per minute). Also, the high rotation speed of the drive motors is reduced in a reduction gear, and the torque on the tool is amplified in an unwanted manner. As the torque of the used motors is often too high, it can be a danger. The thin and highly stressed tools will break because a user cannot transmit dexterity to the mechanical system. The broken tools cannot be left in the tooth, they must be removed through a time-consuming process that often causes the loss of the tooth.

Please replace Paragraph [0031] with the following amended Paragraph:

The neck drive 1 of the Figure 1a, as well as the neck drive 21 of the Figure 2, can be positioned in an angle with respect to a drive part 31 represented in the Figure 3. The drive part 31 has a connection on a drive motor, which is not represented, so that a dental angle piece is created. Also the drive part 31 has a magnetic clutch with clutch parts 32, 33, that can be influenced by a corresponding transmission of the sleeve 13 known from the neck drive 1 of Figure 1. In addition, a reduction gear 34 is provided in the drive part 31 which reduces the high rotation speed produced from the drive motor. As the reduction ~~amplifies~~ increases in a corresponding manner, the torque on the output side, the torque threshold, can be ~~made~~ influenced by means of the magnetic clutch with the clutch parts 32, 33.

Please replace Paragraph [0032] with the following amended Paragraph:

In general, it is accepted that the torque which is transmitted by means of the clutch depends highly from the choice of the magnet material, because different materials of permanent magnets have different magnetic forces. Normally, it is not necessary to use materials with a high magnetic force, because the ~~admitted~~ torques of the treatment tool are relatively small.

Please replace Paragraph [0038] with the following amended Paragraph:

Figure 6 is a chart showing a torque curve for the dependence of the rotation angles between the magnetic clutch parts. The torque M is shown over the rotation angle γ . The diagram begins with an angle position between both clutch parts in a theoretical working point of 90° (zone a) which can arrive for a normal service with a loaded output. The input torque and the output torque are situated inferior to the regulated maximum. In the zone between 0 and $< 180^\circ$ the output torque, which is necessary for the rotation of the treatment tool, is increased. The increase is represented with the curve superior to an angle of 90° . Shortly before equalling a rotation angle of 180° , the highest transmissible torque is equalled for the highest transmissible torque. The magnetic clutch part of the output is stopped. Because of the polarization of the magnetic clutch parts of the input and the output (zone b), a negative output torque occurs when the output continues to rotate, and the reversal of the rotation of the output is reached. In this position, input and output rotate in opposite directions. When the rotation angle of the input continues to increase with respect to the output, the negative output torque re-decreases, and with a rotation angle of 360° the magnets face with their opposite poles. In this position no torque can be transmitted.